16(1)

AUTHORS: Barbashin, Ye.A., and Liberman, L. Kh.

SOV/155-58-3-4/37

TITLE:

On the Stability of the Solutions of a System of Integro-Differential Equations (Ob ustoychivosti resheniy sistemy

integro-differentsial'nykh uravneniy)

PERIODICAL: Nauchnyye doklady vysshey shkoly. Fiziko-matematicheskiye nauki, 1958, Nr 3, pp 18-22 (USSR)

ABSTRACT: '

The author considers the system

(1)
$$\begin{cases} \frac{\partial \varphi(x,u,v)}{\partial u} = \int_{a}^{b} K_{1}(x,s,u,\varphi(s,u,v))ds + F_{1}(x,u,\varphi(x,u,v)) \\ \frac{\partial \varphi(x,u,v)}{\partial v} = \int_{a}^{b} K_{2}(x,s,v,\varphi(s,u,v))ds + F_{2}(x,v,\varphi(x,u,v)), \end{cases}$$

where the functions K_1 , K_2 , F_1 , F_2 in D: $a \le x$, $s \le b$, $0 \le u$, $v \leftarrow + \infty$, $|\phi| \leftarrow r$ belong to the class c_1 , and the auxiliary equations

Card 1/2

 $\frac{d\mathbf{p}(\mathbf{x},\mathbf{u},\mathbf{v})}{d\mathbf{u}} = \int_{0}^{\infty} K_{1}(\mathbf{x},\mathbf{s},\mathbf{u},\boldsymbol{\varphi})d\mathbf{s} + F_{1}(\mathbf{x},\mathbf{u},\boldsymbol{\varphi})$ (2)

AUTHOR:

Liberman, L.Kh.

507/140-58-3-17/34

TITLE:

On the Stability of the Solutions of Integro-Differential Equations (0b ustoychivosti resheniy integro-differentsial'-

PERIODICAL:

Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1958, Nr 3, pp 142-151 (USSR)

ABSTRACT:

The equation

(1)
$$\frac{\partial \varphi(x,t)}{\partial t} = \int_a^b K(x,s,t,\varphi(s,t))ds + F(x,t,\varphi(x,t))$$

is considered, where K and F are defined and continuous in H: $a \le x \le b$, $a \le s \le b$, $|\psi| \le r$, $0 \le t < \infty$; K(x,s,t,0) == F(x,t,0) = 0. With the aid of the contracting mapping it is proved that, if K and F satisfy the Lipschitz condition in φ , (1) possesses a unique solution $\varphi(x,t)$ in the interval $t_0-h < t < t_0+h$ which for $t=t_0$ coincides with a given function f(x) (here it must be $|f(x)| < r_1 < r$ and f(x) is permitted to possess finitely many ordinary discontinuities

Card 1/3

On the Stability of the Solutions of Integro-Differential Equations

SOV/140 -58-3-17/34

in $a \le x \le b$). Besides (1) also the equation

(2)
$$\frac{\partial \varphi(x,t)}{\partial t} = \int_{a}^{b} \overline{K}(x,s,t,\varphi)ds + \overline{F}(x,t,\varphi)$$

is considered, whereby \overline{K} and \overline{F} satisfy the same conditions as K and F and furthermore

$$|\overline{K} - K| < \gamma_1(t) | \varphi(x,t) |$$
, $|\overline{F} - F| < r_1(t) | \varphi(x,t) |$.

Theorem: Let the trivial solution $\Psi = 0$ of (1) be uniformly asymptotically stable; let there exist constants $\alpha > 0$, $B \geqslant 1$, so that

(3)
$$|\varphi(x,t)| < B\delta e^{-dt(t-t_0)}$$
 for $t > t_0$

if $|\phi(x,t_o)| < \delta < r$. Furthermore let

(4)
$$\frac{1}{T} \int_{t}^{t+T} \gamma_{1} dt < \gamma_{1}, \frac{1}{T} \int_{t}^{t+T} r_{1} dt < \gamma_{2}$$
, where $T = \frac{1}{\alpha} \ln 4 B$

Card 2/3

On the Stability of the Solutions of Integro-Differential Equations

SOV/140-58-3-17/34

Then the trivial solution $\varphi=0$ of (2) is uniformly asymptotically stable too, and every solution of (2) satisfies an inequality of the type (3).

Under similar assumptions a third theorem says that from the uniform asymptotic stability of the trivial solution of (1) follows the uniform asymptotic stability of the trivial solution of the "disturbed" system (2), if only the disturbances are small in the mean i.e. if they satisfy conditions of the type (4).

There are 4 Soviet references.

ASSOCIATION: Ural'skiy politekhnicheskiy institut imeni S.M. Kirova (Ural Polytechnic Institute imeni S.M.Kirov)

SUBMITTED:

October 31, 1957

Card 3/3

AUTHOR:

Liberman, L.Kh.

SOV/140-58-6-16/27

TITLE:

Integro-Differential Equations With a Retarding Argument and the Stability of Their Solutions (Integro-differentsial'nyye uravneniya s zapazdyvayushchim argumentom i ustoychivost'ikh resheniy)

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1958, Nr 6,

pp 161-175 (USSR)

ABSTRACT:

The author considers the equation

$$\frac{\partial \varphi(x,t)}{\partial t} = \int_{a}^{b} K[x,s,t,\varphi(s,t-T_{1}(t)),...,\varphi(s,t-T_{n}(t))] ds+$$

+
$$F[x,t, \varphi(x,t-\overline{C}_1(t)),..., \varphi(x,t-\overline{C}_n(t))]$$
.

The proved theorems generalize the results obtained in an earlier paper of the author [Ref 1] and they are analogous to the assertions of Repin [Ref 2] for ordinary differential equations with a retarding argument. The most essential result of the paper are the estimations obtained for the change of the solution for the variation of the functions K and F. Ten long theorems and lemmas are formulated.

Card 1/2

There are 3 Soviet references.

CIA-RDP86-00513R000929810(**APPROVED FOR RELEASE: Monday, July 31, 2000**

"APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000929810

Integro-Differential Equations With a Retarding Argument SOV/140-58-6-16/27 and the Stability of Their Solutions

ASSOCIATION: Ural'skiy politekhnicheskiy institut imeni S.M.Kirova (Ural Polytechnical Institute imeni S.M.Kirov) SUBMITTED: February 17, 1958

Card 2/2

APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000929810(

energy say

8

16(1)

Liberman, L. Kh.

soy/140-59-1-9/25

AUTHOR: TITE

On the Question of Stability of the Solutions of Integro-Difference Equations (K voprosu ob ustoychivosti resheniy

integro-raznostnykh uravneniy)

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Matematika, 1959,

Nr 1, pp 91-104 (USSR)

ABSTRACT:

Beside of the integro-differential equations

(1)
$$\frac{\partial \varphi(x,t)}{\partial t} = \int_{B}^{b} K(x,s,t,\varphi(s,t))ds + F(x,t,\varphi(x,t))$$

the author considers the integro-difference equations

(2)
$$\Delta \varphi_{i}^{h} = h \left[\int_{a}^{b} K(x,s,h,t_{i},\varphi^{h}(s,t_{i})) ds + F(x,h,t_{i},\varphi^{h}(x,t_{i})) \right]$$

He investigates the connection between the behavior of stability of the solutions of (1) and (2), especially conditions under

Card 1/2

APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000929810(

On the Question of Stability of the Solutions

of Integro-Difference Equations

which the stability of the solution remains preserved for the

which the stability of the formulated theorems are similar

transition from (1) to (2). The formulated theorems are similar

to those of Skalkina Ref 1,2 on the stability of difference

equations.

There are 4 Soviet references.

ASSOCIATION:Ural'skiy politekhnicheskiy institut imeni S.M.Kirova (Ural

Polytechnical Institute imeni S.M.Kirov)

SUBMITTED: March 3, 1958

Card 2/2

69767 8/155/59/000/02/008/036

16.3900 16.6500

AUTHOR: Liberman, L.Kh.

.Kh.

TITLE: On the Conservation of the Stability Property of the Solution of an Integro-Difference Equation Under Variation of the Step Width

PERIODICAL: Nauchnyye doklady vysshey shkoly. Piziko-matematicheskiye nauki, 1959, No. 2, pp. 46-48

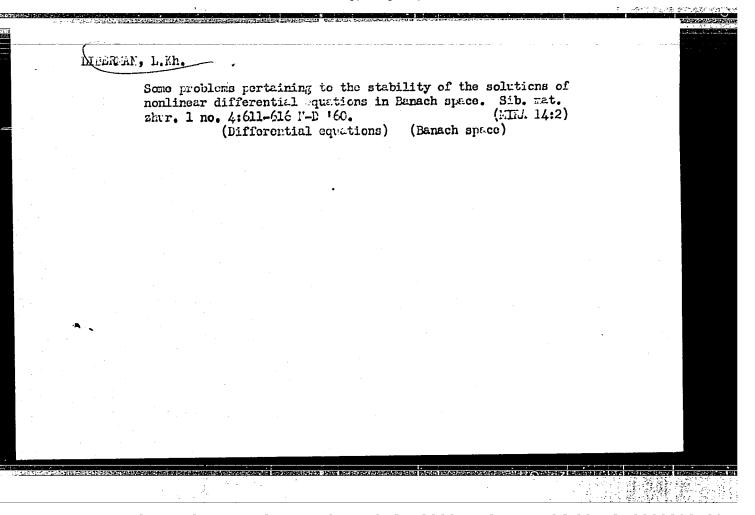
TEXT: Let the equations

(1)
$$\varphi_{i+1}^{h}(x) - \varphi_{i}^{h}(x) = h \left[\int_{a}^{b} K(x,s,h,t_{i}^{h},\varphi_{i}^{h}(s))ds + F(x,h,t_{i}^{h},\varphi_{i}^{h}(x)) \right]$$
 be given

where it is $\varphi^h(x) = \varphi^h(x,t_1)$, and (2) which arises from (1) by taking the new step 1 (0<1<h) instead of h. Let K and F be defined in D $\{a \le x \le b, a \le s \le b, |\psi| \le r, 0 \le h \le \overline{h}, 0 \le t \le \omega\}$ and continuous; $\frac{\partial K}{\partial \varphi}$, $\frac{\partial F}{\partial \varphi}$ bounded

in D; $\frac{\partial K}{\partial t}$, $\frac{\partial F}{\partial t}$, $\frac{\partial F}{\partial h}$, $\frac{\partial F}{\partial h}$ are assumed to satisfy the Lipschitz condition in Card 1/2

APPROVED FOR RELEASE. Monday, July 31, 2000



45111

s/199/63/004/001/004/005 B112/B102

AUTHOR:

Liberman, L. Kh.

The stability of retarded differential operator equations with respect to perturbations confined on the average TITLE:

Sibirskiy matematicheskiy zhurnal, v. 4, np. 1, 1963, 138-144 PERIODICAL:

TEXT: The operator equation $dx/dt = f(x(t - \tau_i(t)), t)$ (i = 1, 2, ...,

(1) is considered under the assumptions that f(x,t) is continuous with respect to t and satisfies the Lipschitz condition

(2) $||f(x'(t-\tau_{I}(t)), t)-f(x''(t-\tau_{I}(t)), t)|| \leq L \sum_{i=1}^{n} ||x'(t-\tau_{I}(t))-x''(t-\tau_{I}(t))||.$

with respect to x, and that f(0,t) = 0. By means of a continuous and bounded linear mapping ϕ a Banach space X containing an operator \overline{f} is associated with the Banach space X containing the operator f. It is shown that the trivial solution of the equation $d\bar{x}/dt = f(\bar{x}(t-r_i(t)), t)$ (i = 1, 2, ..., n) (5) is stable against perturbations small on the average

Card 1/2

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000929810

The stability of retarded	S/199/63/004/001/004/ B112/B102 e equation (1) is uniformly asymp	
if the trivial solution stable, and if an inequality $\int f(\varphi, x(t), t) - \varphi^{-1}f(x(t), t)$ and is small on the average. SUBMITTED: November 24, 1960	t) \ \(\(\(\(\) \) \) \(\) \(\(\) \) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\) \(\)) is integrable
Card 2/2		

ACCESSION NR: AP4039629

\$/0140/64/600/003/0088/0092

AUTHOR: Liberman, L. Kh. (Sverdlovsk)

TITLE: Problems in the theory of approximate solutions of differential operator equations in Hilbert space

SOURCE: IVUZ. Matematika, no. 3, 1964, 88-92

TOPIC TAGS: approximate solution theory, differential operator equation, Hilbert space, nonlinear equation, nonlinear operator, control, mean square deviation

ABSTRACT: Let f(x) and $\phi(c_1,...,c_m,u_1(t),...,u_n(t),t)$ be nonlinear operators satisfying certain conditions; $x,u_1,...,u_n$, for given t, are elements of Hilbert space; $c_1,...,c_m$ are numbers. The author studies some problems in the theory of approximate solutions of nonlinear differential-operator equations of the form

$$\frac{dx}{dt} = f(x, t) + \varphi(c_1, \dots, c_m, u_1(t), \dots, u_n(t), t), \qquad (1)$$

Card 1/2

LIBERMAN, L.L.

Testing small concentrations of insulin by means of the isolated epididymal fat from a rat. Biul. eksp. biol. i med. 52 no.7:121-124 Jl '61. (MIRA 15:3)

1. Iz endokrinologicheskoy laboratorii (nauchnyy rukovoditel' deystvitel'nyy chlen AMN SSSR V.G. Baranov) Instituta akusherstva
i ginekologii (direktor - chlen-korrespondent AMN SSSR prof.
P.A. Beloshapko [deceased]) AMN SSSR, Leningrad. Predstavlena
deystvitel'nym chlenom AMN SSSR V.G. Baranovym.

(INSULIN)

(ADIPOSE TISSUES)

LIBERMAN, L.L. (Kokhtla-Yarve)

Problem of insulin-resistant forms of diabets mellitus. Problemdok. 1 gorm. 2 no.4:88-89 Jl-Ag 156. (MLRA 9:11)

1. Iz endokrinologicheskogo kabineta i terapevticheskogo otdeleniya gorodskoy bol'nitsy g. Kokhtla-Yarve (glavnyy vrach B.K. Volkov) Estonskoy SSR.

(INSULIN, therapeutic use, diabetes mellitus, regist. (Rus))

LIBERMAN L. L. (Kokhtla-Tarve).

Effect of respiratory insufficiency on basal metabolism. Probl. endokr. 1 gorm. 4 no.5:60-67 S-0 '58. (MIRA 11:12)

1. Is laboratorii osnovnogo obmena gorodskoy bolinitsy Kokhtla-Yarve Estonskoy SSR (glavnyy vrach A.D. Zhdanova), nauchnyy rukovoditeli raboty - doktor med. nauk A.G. Dembo. (RESPIRATION,

insuff., eff. on basal metab. (Rus))
(RASAL METABOLISM, physicl.
eff. of resp. insuff. (Rus))

LIBERMAN, L.L.

Pulmonary respiratory function in thyrotoxicosis. Vrach.delo no.7 747 J1 158 (MIRA 11:9)

1. Gorodskaya bol'nitsa g. Kokhtla-Yarva Estonskoy SSSR (nauchnyy rukovoditel' - doktor med. nauk A.G. Dembo).

(RESPIRATION)

(THYROID GLAND-DISEASES)

LIBERHAN L.L.

Insufficiency of external respiration in cardiovascular diseases. (MIRA 11:9) Terap.arkh. 30 no.8:24-32 Ag '58

1. Iz gorodskoy bol'nitsy Kokhtla-Yarve Estonskoy SSR (glavnyy vrach A.D. Zhdanova, nauchnyy rukovoditel' raboty - doktor med.nauk A.G. Dembo).

(CARDIOVASCULAR DISEASES, physiol.

resp. (Rus))
(HESPIRATION.

insuff. in cardiovasc.dis. (Rus))

LIBERMAN, L. L.: Master Med Sci (diss) -- "The function of external respiration and basal metabolism in patients with throtoxicosis, and chronic cardiovascular and pulmonary diseases". Leningrad, 1959. 22 pp (Acad Sci USSR, Inst of Physiology im I. P. Pavlov), 150 copies (KL, No 8, 1959, 138)

LIBERMAN, L.L.

Vital capacity, maximum ventilation of the lungs and reserve ventilation as functional indexes of external respiration. Vrach.delo no.6: 617-630 Je '59. (MIRA 12:12)

1. Gorodskaya bol'nitsa g. Kokhtla-Yarve (Estonskaya SSR). (RESPIRATION)

LIBERMAN, L.L.

Spirographic study of patients with disorders of thyroid gland function. Probl. endok. i gorm. 6 no.6:43-47 '60. (MIRA 14:2) (THYROID GLANL-DISEASES) (SPIROSCOPY)

LIBERMAN, L.L.

Hyperventilation syndrome. Sov.med. 24 no.3:52-55 Mr '60.

1. Iz Gorodskoy bol'nitsy g. Kokhtla-Yarve (glavnyy vrach A.D.Zhdanova)

Estonskoy SSR.

(RESPIRATION)

MBMBO, A.G., prof.; LIBERMAN, L.L., kand.med.nauk (Leningrad)

Ourrent status of the problem of hypertension of the lesser circulation; survey of foreign literature. Terap.arkh. 32 no.9:3-14 160. (MIRA 14:1) (HYPERTENSION) (PULMONARY ARTERY—DISEASES)

DEMBO, A.G., prof.; LIBERMAN, L.L., kand.med.nauk (Leningrad)

Glassification of respiratory insufficiency; survey of the
literature. Terap.arkh. 33 no.313-11 Mr '61. (MIRA 14:3)

(RESPIRATORY ORGANS—DISEASES)

LIBERMAN, L.L.; DRIZGALOVICH-YEGOROVA

Insulin activity of the blood plasma in young and newborn rabbits in alloxan diabetes produced at various stages of pregnancy. Biul. eksp. biol. i med. 53 no.2:63-66 F '62. (MIRA 15:3)

l. Iz endokrinologicheskoy laboratorii (nauchnyy rukovoditel' - deystvitel'nyy chlen AMN SSSR prof. V.G. Baranov) i patofiziologicheskiy laboratorii (zav. - prof. N.L. Garmasheva) Instituta akusherstva i ginekologii (dir. - prof. M.A. Petrov-Maslakov) AMN SSSR, Leningrad. Predstavlena deystvitel'nym chlenom AMN SSSR V.G. Baranovym.

(INSULIN)
(PREGNANCY, COMPLICATIONS OF)

(DIABETES) (ALLOXAN)

LIBERMAN, L.L.; DMITFENKO, L.V.; Prinimal uchastive MAROSHEVSKIY, Yu.A.

Isolation of substances with insulin activity from the blood plasma and urine with the aid of ion-exchange resins. Vop. med. khim. 8 no.4:420-423 Jl-Ag :62.

(MIRA 17:11)

1. Endokronologicheskaya laboratoriya Instituta akusherstva i ginekologii AMN SSSE i laboratoriya kolloidnoy khimii Instituta vysokomolekulyarnykh soyedineniy AN SSSR, Leningrad.

RASKIN, A.M. (Leningrad); LIHERMAN, L.L. (Leningrad)

Role of male and female sex hormones in the origination and

maintenance of the sexual instince in women. Trudy Gos. nauch.
issl. psikhonevr. inst. 29:359-367 '63. (MIRA 17:8)

LIBERMAN, L.L. (Leningrad)
Insulin activity of the blood. Usp. sovr. biol. 55 no.2:296[MIRA 17:8]
312 163.

BARANOV, V.G.; LIBERMAN, L.L.; RASKIN, A.M. (Leningrad)

Diabetes mellitus in pregnancy. Sovr. vop. endok. no.2:214-239
Sovr. vop. endok. no.2:214-239 '63. (MIRA 12:9)

1. Institut akusherstva i ginekologii AMN SSSR, Leningrad.

LIBERIAN, L.L. Separation of free and bound innolin in blood plasma on the exchange resins. Vop. med. knim. To no.1:80-83 Ja-F loi. (NEW 17:12) 1. Laboratory of Encocrinology, Institute of Obstetrics and Gynecology, Academy of Medical Sciences of the U.S.S.R., Uningrad.

BARANOV, V.G., prof.; LESHCHINSKAYA, A.F.; LIBERHAN, L.L., kand. med. nauk; SAMSONOVA, N.K.; SHNEYDERMAN I.M.

Incidence of diabetes mellitus according to a survey of the Leningrad population. Sov. med. 28 no.4:57-61 Ap '64. (MIRA 17:12)

l. Iahoratoriya vozrastnoy fiziologii i patologii cheloveka Instituta fiziologii AN SSSR i endokrinologicheskiy otdel Instituta akusherstva i ginekologii AMN SSSR, Leningrad. 2. Deystvitel'nyy chlen AMN SSSR (for Baranov).

LIBERMAN, L.L.; YAROSHEVSKIY, Yu.A.

Insulin function of the mother and fetus. Biul. eksp. biol.
i med. 56 no.8:21-24 Ag 163.

(MIRA 17:7)

1. Iz endokrinologicheskoy laboratorii (nauchnyy rukovoditel - deystvitel nyy chlen AMN SSSR prof. V.G. Baranov) Instituta akusherstva i ginekologii (direktor - prof. M.A. Petrov - Maslakov) AMN SSSR, Leningrad. Predstavlena deystvitel nym chlenom AMN SSSR V.G. Baranovym.

LIBERMAN, L.L.

Regulation of the insular function in man. Fiziol.zhur. 50 no.6:750-755 Je *64. (MIRA 18:2)

1. Otdel endokrinologii Instituta akusherstva i ginekologii AMN SSSR, Leningrad.

LIBERMAN, L.L., kand. med. nauk

Insulin activity of the blood and urine in hyperinsulinism. Vest. khir. 93 no.9:25-28 S '64. (MIRA 18:4)

1. Iz endokrinologicheskoy laboratorii (nauchnyy rukovoditel'prof. V.G.Baranov) Leningradskogo instituta akusherstva i ginekologii AMN SSSR.

LIBERMAN, L.L.

Formation of insulin and problems of the pathogenesis of diabetes mellitus; survey of the literature. Probl. endok. i gorm. 11 no.1: 119-127 Ja-F '65. (MIRA 18:5)

1. Otdel endokrinologii (nauchnyy rukovoditel' - prof. V.G. Baranov) Instituta akusherstva i ginekologii (dir. - prof. M.A. Petrov-Masla-kov) AMN SSSR, Leningrad.

LIBERMAN, L.L.

Two fractions of blood insulin and their physiological equilibrium. Ukr. biokhim. zhur. 37 no.3:447-454 '65. (MIRA 18:7)

1. Otdel endokrinologii Instituta akusheratva i ginekologii AMN SSSR, Leningrad.

LIBERMAN, L.L.; RASKIN, A.M.; SAVCHENKO, O.N.; STEPANOV, G.S.

Mechanism of depressed sexual development in women with congenital virilizing adrenocortical hyperplasia. Probl. endok. i gorm. 10 no.4:13-17 Jl-Ag 64. (MIRA 18:6)

1. Laboratoriya endokrinologii (nauchnyy rukovoditel' - deystvitel'nyy chlen AMN SSSR prof. V.G.Baranov) Instituta akusherstva i ginekologii (dir. - prof. M.A.Petrov-Maslakov) AMN SSSR i laboratoriya vozrastnoy fiziologii i patologii endokrinnoy sistemy cheloveka (zav. - deystvitel'nyy chlen AMN SSSR prof. V.G.Baranov) Instituta fiziologii imeni Pavlova (dir. - akademik V.N.Chernigovskiy) AN SSSR, Leningrad.

BARANOV, V.G.; LIBERMAN, L.L.; SOKOLOVEROVA, I.M.

Some fundamental problems of the pathogenesis of diabetes mellitus. Vest, AMN SSSR 20 nc.10:35-47 165.

(MIRA 18:10)

1. Institut fiziologii imeni I.P.Pavlova AN SSSR i Vnstitut akusherstva i ginekologii AMN SSSR. Leningrad.

LIBERMAN, L.L.

Case of clinical remission of diabetes. Probl. endok. i gorm.
11 no.6:49-50 N-D *65. (MIRA 18:12)

1. Otdel endokrinologii (nauchnyy rukovoditel' - deystvitel'nyy chlen AMN SSSR prof. V.G. Baranov) Instituta akusherstva i ginekologii (dir. - chlen-korrespondent AMN SSSR prof. M.A. Petrov-Maslakov) AMN SSSR, Leningrad.

YANSON, V.M.; LIHERMAN, L.M.

Selection of clearances and fits for bearings made of polycaprolactsm. Plast, massy no.2:51-56 '61. (MIRA 14:2) (Hexamethylenimine) (Bearings (Machinery))

8/653/61/000/000/007/051 I042/I242

AUTHOR: Liberman, L.M.

TITLE: The application of plastics in agricultural machinery

SOURCE: Plastmassy v mashinostroyenii i priborostroyenii.
Pervaya resp. nauch.-tekh. konfer. po vopr. prim.
plastmass v mashinostr. i priborostr., Kiev, 1959.

Kiev, Gostekhizdat, 1961, 68-73

TEXT: The Latviyskaya ccl'skokhozyaystvennaya akdemiya (Latvian Agricultural Academy) is making efforts to introduce plastics into the construction of agricultural machinery in order to economize on bronze, cut down on weight, and simplify production. Polycaprolactame (caprone) has already been used with success in bearings which do not require lubrication. The advantages of this arrangement are outlined. The procedure for casting caprone parts is given. Various

Card 1/2

S/653/61/000/000/007/051 1042/1242

The application of plastics....

field tests of caprone bearings, bushings, and nuts, are described. Caprone bearings require a relatively large clearance to allow for expansion. Formulas for calculating the size of these clearances are given. A survey of Riga factories manufacturing caprone parts revealed that dimensional accuracy varies between the 4th and 5th class of foot (GOST). There are 2 tables.

Card 2/2

KLIMS, E.P.; LIBERMAN, L.M.; PRIYEDITIS, D.B.

Depositing powdered plastics in a vibrating fluidized bed.
Plast.massy no.7:35-37 '62. (MIRA 15:7)

(Protective coatings)

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000929810

		DECEASED		7041.	
LI HERMAN, L.	M•		-	1964	
METALLURGY		C• 163			
			,		
				-	
		erakan Merilian di Kembana di Kem Menjangkan di Kembana d			
			e de la companya de La companya de la co		

THE SECOND SECOND PROPERTY OF THE SECOND					
		THE COLUMN TWO IS NOT THE PROPERTY OF THE PROP			

P. LIBERMANN, Lucy

Psychological institutions in Rome. Magy pszichol szemle 17 no.2:207-209 160.

1. Budapesti Orvostudomanyi Egyetem I.sz. Gyermekklinikaja; Magyar Tudomanyos Akademia Pszichologiai Bizottsaga Modszertani Albizottsaga elnoke; "Magyar Pszichologiai Szemle" szerkeszto bizottsagi tagja.

.

AUTHOR:

LIBERMAN, L.S.

109-7-15/17

A Method of Voltage Standing-Wave Ratio Measurement of Videode-

teotors. (Metod izmereniya KSVN videodetektorov, Russian) Radiotekhnika i Elektronika, 1957, Vol 2, Nr 7, pp 941-942

(U.S.S.R.)

ABSTRACT:

PERIODICAL:

These measurements have to be undertaken at a very low efficiency level. At such levels, however, the usual line of measurements, especially within the millimeter wave domain, is full of grave errors. Besides, the "uncoupling" desired on the occasion of such changes according to the generator from

5 - 10 db cannot always be warranted.

These difficulties are eliminated if the method worked out here is used. If the load phase is changed by means of the pressure line, the highest and the lowest value of the rectified current can be obtained which would correspond to the highest and lowest decline of power.

For the method described here a power level of less than 1 μ W would be sufficient, and no uncoupling attenuator would be

Card 1/2

A Method of Voltage Standing-Wave Ratio Measurement of Videode-

necessary.

The amplifier 28-I was used as an indicator of the rectified current. (With 1 Illustrations).

ASSOCIATION:

Not given

PRESENTED BY:

SUBMITTED:

AVAILABLE:

Library of Congress

Card 2/2

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000929810

SOV/115-59-5-22/27

8(3), 9(3) AUTHOR:

Liberman, L.S.

TITLE:

Measuring of a Generator's Reflection Factor with a Phase Rotator

PERIODICAL:

Izmeritel'naya Tekhnika, 1959, Nr 5, pp 52-53 (USSR)

ABSTRACT:

The author presents a method of measuring a generator's reflection factor with a phase rotator instead of a transformer (Fig.1) Ref.1. The source of power is linked with the detector through a phase rotator. The article gives the calculation of the dependence between the dimishing of power and phase of the reflection factor. The calculation gives the possibility of measuring the reflection factor by measuring the maximum and minimum rectified current (or voltage) of a phase rotator. The method is suitable for measuring a broad range of waves, provided that the condition $G_n=1$ ($G_n=reflection$ factor of the load) is accomplished. There are 1 layout, 2 equations and 3 Soviet references.

Card 1/1

LIBERMAN, L.S.

Growth of a p-n junction breakdown voltage at superhigh frequencies. Radiotekh. i elektron. 8 no.10:1795 0 '63. (MIRA 16:10)

A FISSION NR AT5004891

5/2657/64/000/012/0032 0057

621.382.014.2

AUTHOR: Sestroretskiy, B. V.; Liberman, L. S.

|| |5+1 |

TITLE: Theory of shf semiconductor-diode switches

SOURCE: Poluprovodnikovyye pribory i ikh primeneniye; sbornik statey, no. 12, 1964, 32-57

TOPIC TAGS: semiconductor diode, semiconductor diode switch

is des actuals de la companya de la

ABSTRACT: A general method of analysis of shf semiconductor-diode switches a proposed. One-diode switches are considered, and optimal conditions for a switch operating at a specified frequency are found. The power is switched by changing the capacitance and resistance of the p-n junction by application of an extract voltage. By regarding the one-diode switch as a reversible reactive considerate work, general formulas if the capacitans. The relation (4.)

Cord 1/2

"APPROVED FOR RELEASE: Monday, July 31, 2000

CIA-RDP86-00513R000929810

L 55425-65

ACCESSION NR: AT5004891

2

between the above losses characterizes the switch performance. The performance-determining parameters can be measured if the diode is tested under these three conditions: no-load, short-circuit, and a definite load. Orig. art. has: 13 figures and 78 formulas.

arti mani 13 mgaron and 10 marin

ASSOCIATION: none

SUBMITTED: 00

ENCL: 00

SUB CODE: EC

NO REF SOV: 000

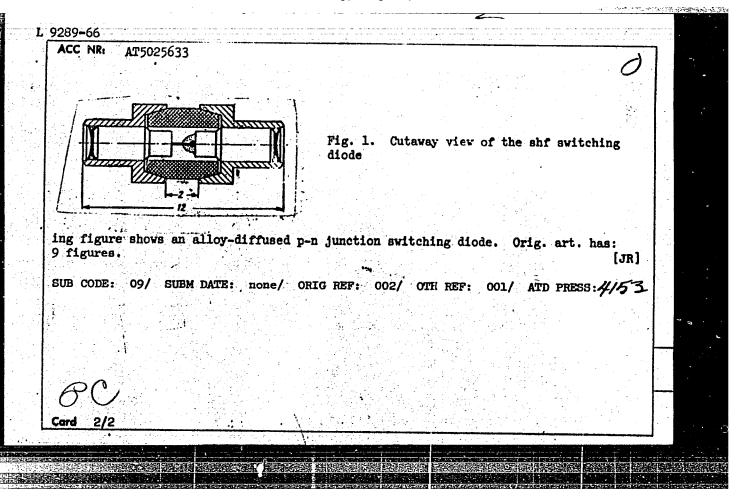
OTHER: 000

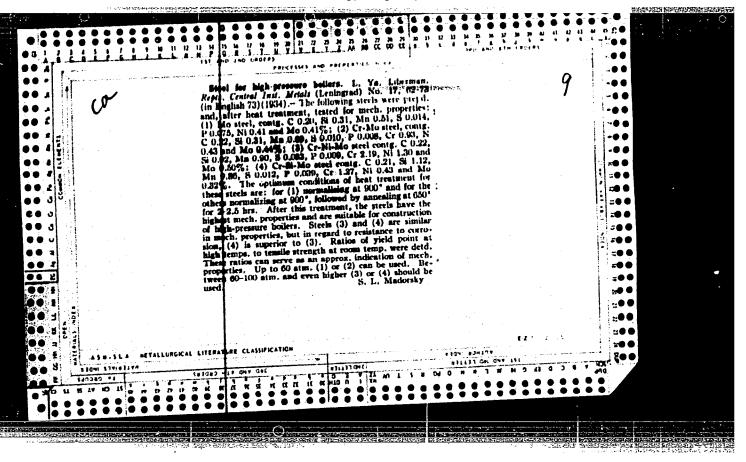
Card 2/2

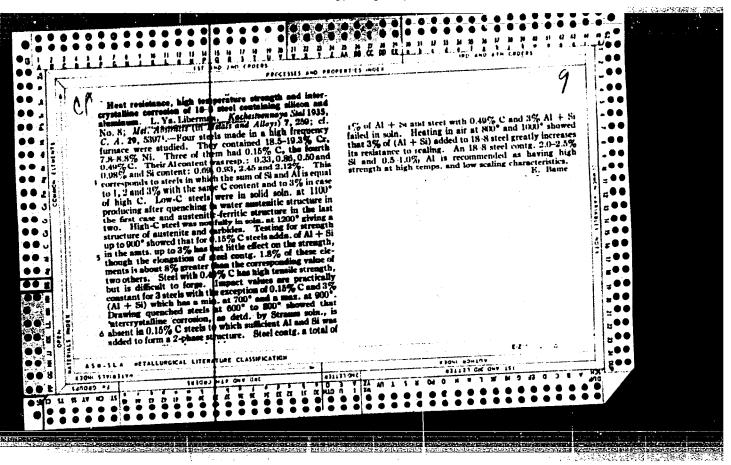
"APPROVED FOR RELEASE: Monday, July 31, 2000

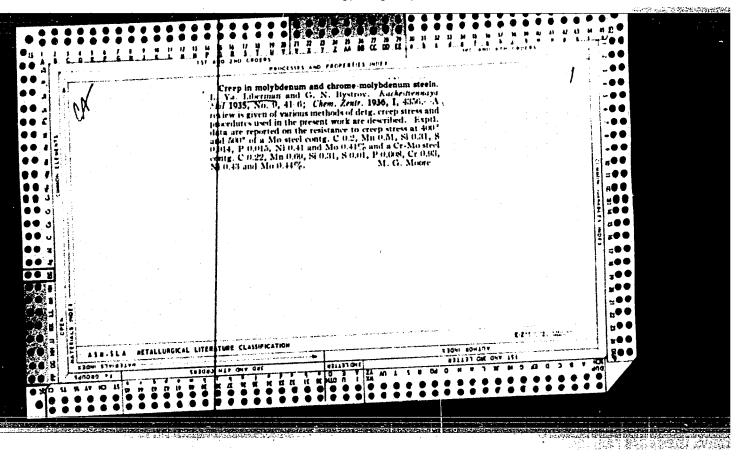
CIA-RDP86-00513R000929810

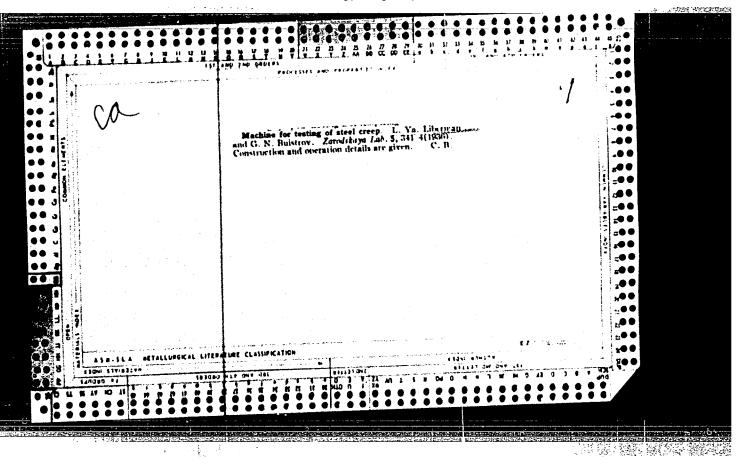
EWT(1)/EWT(m)/EEC(k)-2/T/EWP(t)/EWP(b)/EWA(b)ACC NR AT5025633 SOURCE CODE: UR/2657/65/000/013/0003/0022 Liberman, L. S. ORG: none TITLE: Shf p-n junction switching diodes SOURCE: Poluprovodníkovyye pribory i ikh primeneniye; sbornik statey, no. 13, 1965. 3-22 TOPIC TAGS: semiconductor diode, junction diode, germanium diode, switching circuit, pro junction ABSTRACT: Descriptions are given of the general operation of p-n junction germanium diodes used in switching circuits and of a new type of shf germanium diode based on the resonance principle. The new switching diode is designed for operation in the microwave region and has the following parameters: transmission losses, less than 0.2 db; cutoff, higher than 30 db; and switching time, 20 nanosec. Due to the small interelectrode gap, the breakdown voltage does not exceed 200 v, thus limiting the amplitude of shf signals which can be manipulated by the diode. In this respect, p-n junction diodes with a thin base are inferior to diodes with a p-i-n structure, because the latter can operate at a higher shf power (e.g., 1-10 kw). However, p-i-n diodes have a longer switching time and consequently a lower Q. The accompany-Card 1/2 UDC: 621.382.2.029.64

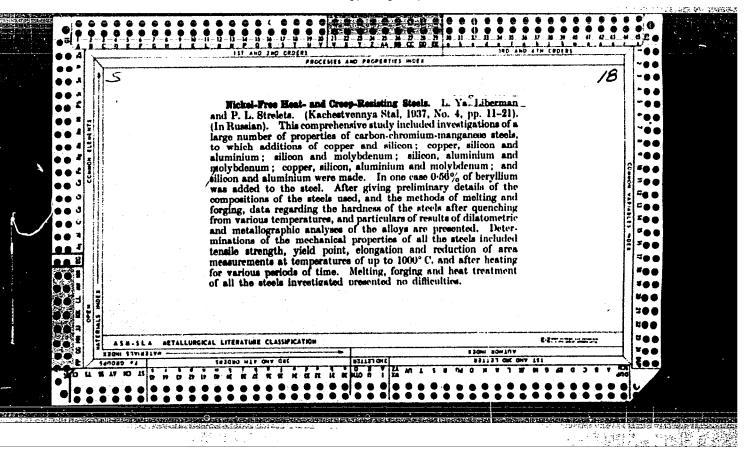


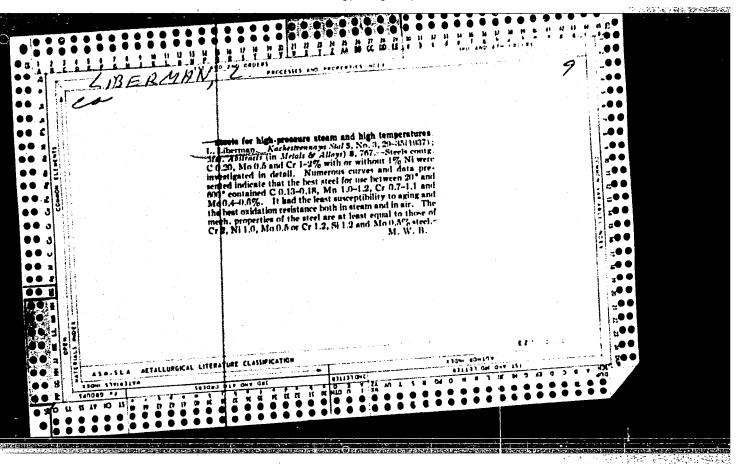


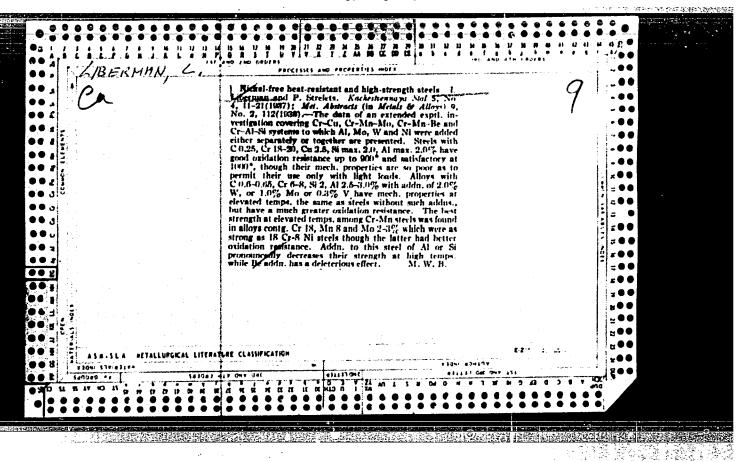


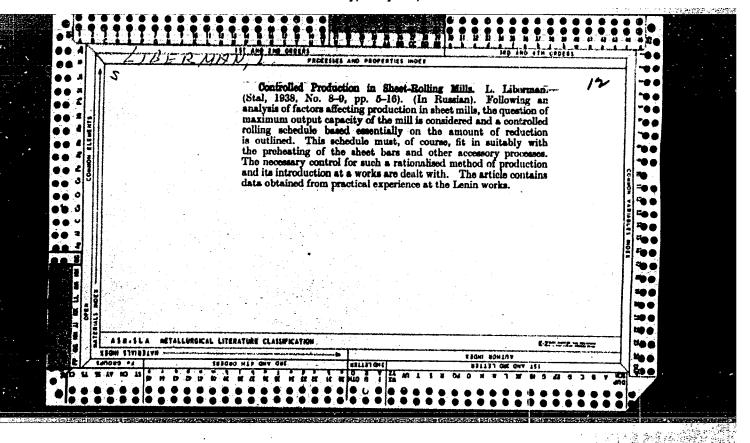












18(0)

PHASE I BOOK EXPLOITATION

sov/1936

Liberman, L. Ya., Candidate of Technical Sciences, and M.I. Peysikhis, Engineer.

Spravochnik po svoystvam Staley, primenyayemykh v Kotloturbostroyenii (Handbook on Properties of Steels Used in Boiler and Turbine Construction) 2d ed., enl. Moscow, Mashgiz, 1948. 408 p. (Series: Tsentral'nyy nauchno-issledovatel'skiy kotloturbinnyy institut. [Izdaniya] km. 32) Errata slip inserted. 8,500 copies printed.

Sponsoring Agency: Tsentral'nyy nauchno-issledovatel'skiy kotloturbinnyy institut.

Ed.: A.A. Kanayev, Candidate of Technical Sciences; Tech. Ed.: P.G. Pol'skaya.

PURPOSE: This handbook is intended for designers, physical metallurgists, metallurgists, metallurgists of boiler and turbine plants, and also personnel of plant laboratories and scientific research institutes of other branches of machine building.

COVERAGE: This is the second edition of a handbook on boiler and turbine steels originally published in 1955. The present edition describes 90 types of steels,

Card 1/9

Handbook on Properties (Cont.)

sov/1936

and is based exclusively on experimental material obtained during the past several years at various Soviet scientific research institutes and plant laboratories. Contributions from TsKII (Central Committee for Heavy Industry), TsNIIMASh (Central Scientific Research Insitute of Heavy Machinery), TsNIIchM (Central Scientific Research Institut of Ferrous Metallurgy), and the laboratories of the Leningradskiy metallicheskiy zavod (Leningrad Metal Plant), Khar'kovskiy turbinnyy zavod (Khar'kov Turbine Plant), Nevskiy machinostroitel'nyy zavod (Neva Machine-building Plant), and the Novo-Kramatorskiy metallurzicheskiy zavod (New Metallurgical Plant in Kramotorsk) are represented. The handbook covers systematically the whole range of materials from carbon steels to the most heat-resistant high-alloy and nonferrous metals used at present, or which may be used in the near future, in manufacturing boiler and steam- and gasturbines. The authors say that all available information for each type of steel on mechanical properties, stability of properties at various temperatures, data on creep-resistant and creep-rupture properties, and design graphs for selecting design stresses and strains are presented. For those steel types which are intended for fastening parts of boiler and turbine units, stress-relaxation characteristics are also presented. The handbook includes existing GOST (All-Union State Standards) and Technical Specifications for materials used in boiler and turbine making. The thermal conductivity coefficients experimentally determined by Engineer R.Ye, Krzhizhamovskiy, TsKII, and not included in the first edition for many types of steel, are given, The authors thank chief specialist on metallurgy Ya.I. Kulandin of the Gosplan Card 2/9

Handbook of Properties (Cont.)	sov/1936
and Department Head Candidate of Technical Sciences A.V. Startheir assistance. There are no references.	nyukovich for
TABLE OF CONTENTS:	
Preface to Second Edition	5
Preface to First Edition	6
Conventional Symbols	8
Ch. 1. Selecting Steel for Continuous Service at High Temperat Determining its Heat-resistant Properties	ture and
Ch. II. Carbon Steels GOST 380-57 normal and improved quality types Type 10 Type 15 Type 20	16 18 21 23 25
Card 3/9	

Handbook of Properties (Cont.) Type 25 Type 30	sov/1936
Type 30	
	29
Type 35	32
Type 40	3 ⁾ ‡
Type 45	39
Types 15K and 20K	31 32 34 39 41
Types 22K and 25K	45
Type 220K steel with increased manganese content	49
Ch. III. Constructional Alloy Steels	· ·
Type 16M	51
Type 12MKh	51
Type 15KhM	57 62
Type 12KhMF	62
Type 12Kh 1MF	66
Type 12Kh2FB	$\frac{71}{26}$
Type EI454	76 70
Type EI531	79 86
Type 16GNM	88
Type 30Kh	90
Types 36KhA and 40Kh	90 92
Type 20KhM	96
Card 4/9	

andbook of Properties (Cont.)	sov/1936
Type 30KhM	101
Type 35KhM and 34KhM	107
Type 35KhMFA	114
Type 25Kh2MFA	118
Type R2	124
Type EI723	130
Type EI415	134
Type 21N5	149
Type 40N	151
Type 4oKhN	154
Type 12KhN3A	156
Type 34KhN3M	158
Type 35KhN3MF	165
Type 50KhFA	169
Туре, 6052	172
Type 38KhMYuA	174
Ch. IV Stainless, Scale-resistant and Hea	t-resistant Steels 177
Types 1Kh13, 2Kh13, 3Hk13, and 4Kh13 sta	
Types 1Kh13 stainless steels	178
	183
Types 2Khl3 stainless steel	

Handbook of Properties (Cont.)	SOV/1936	
Type JKhlJ stainless steel Type 4KhlJ stainless steel Type KhlOS2M(EI107) scale-resistant steel Type 15KhllMF stainless heat-resistant steel Type EI802 (15Khl2VMF) stainless heat-resistant steel Type EI756(iKhl2VMF) stainless heat-resistant steel Type EI756(iKhl2VMF) stainless heat-resistant steel Types IKhl8N9T (EYAIT), and iKhl8N12T stainless steel Types Khl8N11B, and EI724 stainless steel Types Khl8N11B, and EI724 stainless steel Type iKhl4N14V2M (EI257) heat-resistant steel Type iKhl4N14V2MT(EI257 containing titanium) heat-resistant steel Type iKhl3N16B (EI694) heat-resistant steel Type iKhl3N18V2B (EI695) heat-resistant steel Type Khl3N13 scale-resistant steel Type Khl3N18 (EI417) scale-resistant steel Type Khl3N18 (EI417) scale-resistant steel Type EI123 heat-resistant steel Type EI123 heat-resistant steel Type EI572 heat-resistant steel Type EI400 heat-resistant steel Type EI405 heat-resistant steel Type EI405 heat-resistant steel Type EI405 heat-resistant steel	189 193 196 201 204 208 210 217 222 1 228 231 234 237 241 250 255 261 273 281	
Card 6/9	295	
	磁	

The state of the supplementation of the state of the stat		
Handbook of Properties (Cont.)	sov/1936	· · · · · · · · · · · · · · · · · · ·
Type EI424 heat-resistant steel	307	
Type EI612 heat-resistant steel	313	
Type EI612K heat-resistant steel	322	
Type EI434 (KhN10K) heat-resistant steel	32 5	
Type EI388 heat-resistant steel	33 4	
Type EI437 (KhN8OT) heat-resistant alloy	338	
Types EI607 and EI607A heat-resistant alloy	344	
	·	
Ch. V. Steel for Castings	350	
Type 25L cast carbon steel	350	
Type 20KhML alloyed cast steel	354	
Type 20KhMFL alloyed cast steel	359	
Type 26-20 cast scale-resistant steel	365 ·	
Type 1Kh18N9TL heat-resistant cast steel	371,	
Type Kh25N13TL heat-resistant cast steel	373 !	
Types IA1, IA4, and IA5 heat-resistant cast steel	<u> </u>	•
Type IA3 heat-resistant cast steel	380	
Type IA6 heat-resistant cast steel	386	
Ch. VI. GOST and Technical Specifications for Materials Used in		
Boiler and Turbine Making	389	
	309	
Card 7/9		
	ANTERIOR DE LA CARTA DEL CARTA DE LA CARTA DE LA CARTA DEL CARTA DE LA CARTA DEL CARTA DEL CARTA DEL CARTA DEL CARTA DE LA CARTA DEL CARTA DE LA CARTA DE LA CARTA DE LA CARTA DEL	dayr dayras

Carbon sheet-steel for boilers	3 89	
Steels for boiler-tubes, superheaters, collectors, and piping	390	
Steel flanges	391	
Forgings from constructional carbon-and alloy-steel (GOST 8479-57) Chemical composition of steels used for discs, shafts, and all-forged rotors of a steam turbine (in \$) (Standards 1233K, 1234-K and	392	
Technical Specifications of plants)	394	
Forgings for shafts and all-forged rotors of steam turbines	3 95	
Forgings for steam-turbine discs	395	
Chemical composition of steels recommended for making forgings for shafts, all-forged rotors, and discs of steam turbines Standard mechanical properties of forgings for shafts and all-forged rotors of marine and stationary steam turbines	396	
(TUMIM 20-5-54)	397	
Standard mechanical properties of forgings for discs of marine and stationary turbines (TUMTM20-5-54) Blanks for steam-turbine blades heat-treated hot-rolled and	398	
forged from stainless steel (1991K, 1940 standards) Sheets and strips for steam-turbine blade fastening bandages	3 99	
heat-treated cold-and hot-rolled from chromium stainless steel (1392K,1240 Standards)	3 99	
ard 8/9		

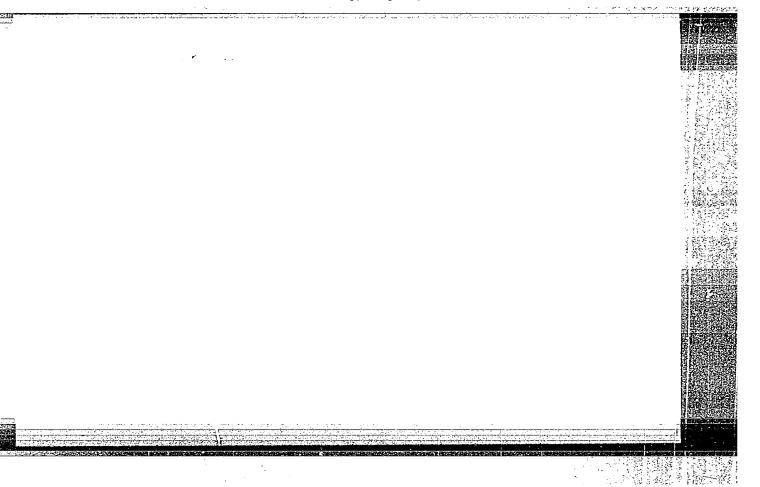
Handbook of Properties (Cont.) (GOST 977-53) carbon steel castings Castings from various types of alloyed steel Welding wire made from GOST 2246-54 type steel Electrodes for welding boiler and turbine steels Electrodes for welding constructional steels Electrodes for welding alloy steels with special properties		SOV/1936 400 401 402 404 407 408	
VAILABLE:	Library of Congress		
!			
ard 9/9		GO/gmp 8-6-59	
•			

LIBERMAN, L.Ya., kandidat tekhnicheskikh nauk.; PEYSIKHIS, M.I., inzhener; KANAYEV, A.A., kandidat tekhnicheskikh nauk, redaktor; POL'SKAYA, R.G., tekhnicheskiy redaktorl

[Handbook on the properties of steels used in marine boiler and turbine building] Spravochnik po svoistva stalei, promeniaemykh v kotloturbostroenii. Moskva, Ges.nauchno-tekhn.izd-vo mashinostrelt. lit-ry, 1955. 195 p. (Leningrad. TSentral'nyi nauchno-issledovatel' skii kotleturbinnyi institut. [Trudy], vel. 29.) (MIRA 9:10) (Steel--Specifications) (Boilers, Marine) (Steam turbines)

LIBERHAN, L.Ya.

Repeated failure test for metals. Zav.lab. 21 no.2:218-222 '55. (MIRA 8:6)



"APPROVED FOR RELEASE: Monday, July 31, 2000 CI

CIA-RDP86-00513R000929810

Category: USSR/Solid State Physics - Mechanical properties of crystals and poly- E-9

crystalline compounds

Abs Jour: Ref Zhur - Fizika, No 1, 1957 No 1363

Author : Liberman, L.Ya., Boyeva, A.V.

Inst : Central Boiler and Turbine Institute, USSR

Title : Heat Resistance and Relaxation Stability of Chrome-Vanadium and Chrome-

Tungsten-Vanadium Structural Steels

1956

Orig Pub: Metallovedeniye i obrabotka metallov, 10, No 4, 2-10

Abstract : An investigation was made to find substitutes for molybdenum-containing

steels, satisfying the requirements imposed on materials for bolts and pins, intended for operation at temperatures up to 500° . A study was made of the effect of the V,W, and C content and its influence on the creep resistance long-term strength, relaxation endurance, and sensitivity to tempering brittleness. It was established that the first three characteristics increase with the vanadium content up to 1%; the maximum sensitivity to tempering and thermal brittleness is displayed by chrome-vanadium steels at 0.5% V. Chrome-vanadium steels containing 1.25% W and 0.25 -- 0.30% C are insensitive to

tempering and thermal brittleness, have high creep resistance, high long-term

Card : 1/2

"APPROVED FOR RELEASE: Monday, July 31, 2000 CIA-RDP86-00513R000929810

Category: USSR/Solid State Physics - Mechanical properties of crystals and poly- E-9

crystalline compounds

Abs Jour: Ref Zhur - Fizika, No 1, 1957 No 1363

strength, and high relaxation endurance. The 25Kh2VlF steel, containing o.23 -- o.30% C, 1.2 -- 1.4% Cr, 1 -- o.4% W and 0.2 -- 0.3% V, has a better combination of properties, satisfying the above requirements.

Card : 2/2

LIEBERMAE, L.Ya., kandidat tekhnicheskikh nauk.

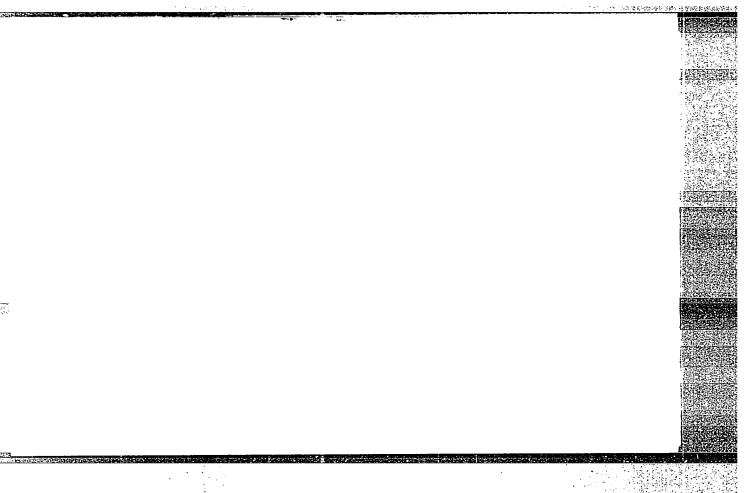
Steel fer steam pewer installations; survey of fereign literature.

Emergemanhinestreenie ne.4:26-30 Ap '56. (MIRA 9:7)

(Steel)

LIBERMAN, L.Ya., kandidat tekhnicheskikh nauk; BOYEVA, A.V., inzhener.

Heat-resisting chromium steels to be used at 550 - 600°. Metalloved. i obr. met. no.6:16-25 Je 156. (MLRA 9:9)



LIBERMAN, L.Ya., kand. tekhn. nauk; PEYSIKHIS, M.I., inzh.; KANAYEV, A.A., kand. tekhn. nauk, red.; POL'SKAYA, R.G., tekhn. red.

[Handbook on properties of steel used in boiler and turbine construction] Spravochnik po svoistvam stalei, primeniaenykh v kotloturbostroenii. Moskva, Gos. nauchno-tekhn. izd-vo mashinostroit. lit-ry, 1958. 408 p. (Leningrad. TSentral'nyi nauchno-issledovatel'skii kotloturbinnyi institut. [Trudy] vol.32)

(Steel)

AUTHOR: Liberman, L. Ya., Candidate of Techn. Sc. 129-2-8/11

TITLE: High Temperature Properties of Austenitic Steels During

Cyclic Temperature Changes. (Zharoprochnye svoystva

austenitnykh staley pri tsiklicheskom izmenenii temperatury)

PERIODICAL: Metallovedeniye i Obrabotka Metallov, 1958, No.2, pp. 38 - 49 (USSR).

ABSTRACT: This is a review of foreign practice, based exclusively on work published in the USA and Great Britain.

There are 16 figures, 9 tables and 15 non-Slavic references.

AVAILABLE: Library of Congress

Card 1/1

LIBERMAN L. Ya. kand. tekhn. nauk

Heat-resistant stoels for power plant applications; based on foreign sources. Energomashinostroenie 4 no.5:44-48 My '58.

(Steel)

(Steel)

LIBERMAN, L.Ta., kand.tekhn.nauk; LEVIN, Ye.Ye., kand.tekhn.nauk

Industrial conference on heat-resistant materials. Energomashinostroenie 4 no.11:40-42 M *58. (MIRA 11:11)

(Refractory materials--Congresses)

18(2)

AUTHOR:

Liberman, L. Ya.

sov/32-24-12-33/45

TITLE:

Parametric Methods for Determining the Endurance of Heat-Resistant Alloys (Parametricheskiye metody dlya otsenki dlitel'noy prochnosti zharoprochnykh splavov)Survey (Obzor)

Zavodskaya Laboratoriya, 1958, Vol 24, Nr 12,

pp 1501 - 1509 (USSR)

ABSTRACT:

PERIODICAL:

In recent years parametric methods of determination have found an ever increasing applicability in testing and interpreting experimental results on endurance. Most used is the parametric function between time, temperature, and tension suggested by Larson and Miller (Refs 1,2). Since the assumption that the energy of activation Q and the time Tare dependent on the tension had not been experimentally confirmed, appropriate experiments were carried out by La Rocca (Lya Rokka) (Ref 3). The observation that the constant C changes from 13 to 14 agrees with the results obtained by N'yukhauz and Van Ullen (Ref 1). Nisbet and Hibbard (Ref 4) found C = 11 in various cobalt

Card 1/3

Parametric Methods for Determining the Endurance of Heat- SOV/32-24-12-33/45 Resistant Alloys .Survey

alloys. Krisch and Wepner (Krish and Vepner) (Ref 5) found that in most cases the parametric function $\sigma = T(C+\lg \tau)$ is expressed by not one but several curves and leads to several values for C in various kinds of steel (Table 1). A comparison table of the experimental and calculated values for the limit of endurance is given (Table 2). From this it is apparent that the error for the majority of the steels varies from +5 to -15%. Bandel et al. (Ref 7) give a diagram for the distribution of the values for the constant C for pearlite and austenite steels (Fig 3). Manson and Brown (Menson and Broun) (Ref 9) determined a linear function lg T-T with o = constant. (T = testing temperature). Orr, Sherby and Dorn (Sherbi) (Ref 11) find a correlation between the test results on creeping and the length of time before decomposition at constant tension and various temperatures and deduce a parameter on the basis of which a parametric function is given in the coordinates o-y for four different materials (Fig 7). Several other sets of data from different authors are given with corresponding tables and diagrams. There are 10

Card 2/3

Parametric Nethods for Determining the Endurance of H_{eat} - SOV/32-24-12-33/45 Resistant Alloys .Survey

figures, 5 tables and 17 references, 2 of which are Soviet.

card 3/3

LIBERMAN, L. Ya., kand. tekhn. nauk

Long-time operational properties of ferrite and austenite pipe and structural steels at high temperatures. Energomeshinostroenie 6 no.6:45-48 Je 160. (MIRA 13:8) (Steel)

LIBERMAN, L.Ya., kand. tekhn. nauk; STANYUKOVICH, A.V., kand. tekhn.

HEUR, red.; LEBEDEVA, N.I., red.; PODCHUFAROVA, S.I., red.;

GROSMAN, L.A., red.; KOVAL'SKAYA, I.F., tekhn. red.

[Materials used in the manufacture of power machinery]Materialy, primeniaemye v energomashinostatoenii. Moskva,
TSINTIMASh, 1961. 181 p. (MIRA 16:4)
(Electric machinery industry—Equipment and supplies)
(Electric engineering—Materials)

20502 S/096/61/000/005/001/003 E111/E552

18.1110

AUTHORS:

Liberman, L. Ya., Candidate of Technical Sciences and

Sokolova, M. N., Engineer

TITLE:

Heat Resisting Steel for Fastenings in Power Installa-

tions

PERIODICAL: Teploenergetika, 1961, No.4, pp.28-34

TEXT: The authors give results of their investigation aimed at finding steels for use as bolts, pins etc. in installations working with steam at 580° C and 240 atm. The properties required are superior to those of type 3N-909 (20×100) (EI-909 (20×100) (EI-909 (20×100) similar to the British steel Durehete 950. The chemical composition of the steels studied and dilatometrically determined critical points are shown in Table 1 (the first column shows the type of steel, X = Kh, M = M, G = F, G = B, B = V, T = T, P = R; the second the heat number and weight in kg; first line gives the permitted range of composition of 20Kh1M1F1 steel). Six of the heats were melted in a 100 kg induction furnace and forged into 70×40 mm or 70 mm diameter blanks; and two in a 500 kg arc furnace and forged to 70 mm diameter blanks. Blanks were annealed at 950° C for two hours

Card 1/6

Heat Resisting Steel for ...

Card 2/6

20502 S/096/61/000/005/001/003 E111/E552

Most heats correspond to the and cooled to 300°C in the furnace. V/C = 4 value shown to be desirable (Ref.2). Steel 20KhlMlFl was taken as the basis, and alloyed as required. A study of the effect of hardening from 950-1050°C and tempering at 650-720°C showed that the properties of all the steels were similar and little affected The carbide electrolytically by differences in heat treatment. separated from the steels heat treated in various ways was weighed and analysed. For the basic steel the amount was little dependent on hardening temperature. With hardening from 950°C the precipitate contained about 0.4% V; with higher hardening temperature the V content was 0.05-0.09. Tempering always led to increase in the amount of precipitate and its iron content while the vanadium content corresponds roughly to the hardened-from-950°C state. X-ray analysis in the refined state shows the carbide phase to be VC with Mo and Fe present. For 20X1M1016 (20Kh1M1F1B) steel in the refined state the amount of iron content of the deposit was greater and the carbide phase was NbC and VC (V content low). With 20XIMIDITP (20KhlMIFITR) steel in the refined state the amount of precipitate is about the same as in the basic steel and the V content is that of the steel itself. With the basic steel double

Heat Resisting Steel for ...

2C502 S/096/61/000/005/001/003 E111/E552

hardening followed by tempering gives a uniform fine structure. Type 20KhlM1F1B contains irregularly distributed ferrite and undissolvedcarbide regions; the third steel differs from the others in having a larger grain of unequal etchability, bainite structure and the presence of primary titanium carbides and carbonitrides. authors concluded from these and other experiments that for their steels oil hardening from 980 or 1000°C and tempering at 700°C to get the required mechanical properties is sound, and used 5-7 hours tempering (yield-point strength 75-80 kg/mm²). All the steels had very similar mechanical and plastic properties at 20-600°C, but 20KhlMlFlTR steel had considerably higher toughness (16-20 kg.m/cm2) than the others (8-15). Tensile tests with various rates of deformation showed that hardening from 980°C gives the best plasticity for 20KhlMlFl and 20KhlMlFlTR steels. No tendency to plasticity for 20KhlMlFl and 20KhlMlFlTR steels. No tendency to temper brittleness was found in any of the steels. The properties of all steels remained satisfactory on prolonged heating for 3000-5000 hours, at 565°C and no important structural changes occurred. Coefficients of linear expansion for 20KhlMlFlTR and 20KhlMlFl steels were measured for various ranges, overall values (20-600°C) being 13.55 and 13.8 (presumably x10 - abstractor), respectively. Card 3/6

Heat Resisting Steel for ...

20502 S/096/61/000/005/001/003 E111/E552

Relaxation properties at 565 and 580°C were studied using the ringtest method of I. A. Oding (not described) and tensile testing cylindrical specimens on yMM-5 (UIM-5) machines. Some differences in results obtained by the two methods were found. Both 20KhlMlFl and 20KhlMlFlTR showed improvement at 565°C with increasing hardening temperature and were better than the other steels; the latter at 580°C has specially high relaxation stability (residual stresses after 10 000 hours are not less than 11 kg/mm²). Fig.4 shows the ratio of residual stress to initial (the "relative relaxation stability") as functions of V:C ratio for 20KhlMlFl steel for various test durations (curves 1-5 correspond to 1000-10000 hours) at 565°C (oil hardening from 1050, tempering at 700°C). Creep tests at 560°C and 12 kg/mm² showed 20KhlMlFlTR steel to be best (11-12 kg/mm² for a creep rate of 10⁻⁵ %/hour); creep for 2000-3000 hours had no appreciable effect on mechanical properties or toughness. Determinations of the long-time strength at 565°C of the steels (of smooth and notched specimens) showed that 20KhlMlFlTR steel is better than the type 9N125(EI723) and 9N45 (EI415) pearlitic steels commonly used for fastenings. This is attributed Card 4/6

20502

eat Resisting Steel for ...

S/096/61/000/005/001/003 E111/E552

to the joint presence of titanium and boron. The authors conclude that 20KhlNlFlTR steel can be used for fastenings (bolts, pins etc.) for prolonged service at metal working temperatures of 565-580°C, and also at lower temperatures when high relaxation stability is needed; the heat-resisting and relaxation properties of 20KhlMlFl steel satisfy its use for fastenings at temperatures up to 565-580°C. There are 6 figures, 7 tables and 4 references: 3 Soviet and 1 non-Soviet.

(Ref.2: Eng. No.4690, 824, 180, 1955).

ASSOCIATION: Tsentral'nyy kotloturbinnyy institut (Central Boiler and Turbine Institute)

Card 5/6

LIBERMAN, L.Ya., kand.tekhn.nauk; SOKOLOVA, M.N., inzh.

Heat-resistant steel for fastening components in electric power systems. Teploenergetika 8 no.5:28-34 My 161. (MIRA 14:8)

1. TSentral'nyy kotloturbinnyy institut.
(Turbines) (Heat-resistant alloys)

1.8000 18 8200 (1413, 1416, 2813) 25357 8/032/61/027/006/008/018 B124/B203

AUTHORS:

Liberman, L.Ya., and Volkova, N.V.

TITLE:

Tests for relaxation and creeping under tensile load

until destruction

PERIODICAL:

Zavodskaya laboratoriya, v. 27, no. 6, 1,61, 724-729

TEXT: The present paper gives the principal results obtained in developing a method of testing the relaxation of stress in one-dimensional elongation of smooth cylindrical specimens under repeated and cyclic load, as well as a method of combined relaxation tests until destruction of the specimens as a method of combined relaxation tests until destruction of the specimens. The authors tested austenitic steel type well (EI612) (0.06% C, 14.9% Cr, 14.9% Cr, 34.92% Ni, 3.68% W, 1.13% Ti), structural steel type 20.1M1\$1 (20Kh1M11) (0.21% C, 1.27% Cr, 1.02% No, 0.84% V), and steel type 28.5% (28KhVFTs) (0.28% C, 1.72% Cr, 0.64% W, 0.64% V, 0.16% Zr); the mechanical properties of these steels are tabulated. In the relaxation tests under repeated load, the specimens were loaded repeatedly to the given initial load for 100 - 1000 hr (sometimes longer). In cyclic relaxation tests, the specimen was 10 aded to the initial stress for 100 hr each until its destruction. The Card 1/9

25357

S/032/61/027/006/008/018 B124/B203

Tests for relaxation ...

relaxation stability rises with repeated loading. For studying the effect of previously accumulated plastic deformation on stress relaxation, the method of combined testing for relaxation and creeping was used instead of cyclic relaxation, in which the specimen had previously been in the condition of isothermal creeping at constant nominal stress until reaching the given plastic deformation of 0.1 - 1.0%. After reaching it, the specimen was released and tested for relaxation at the same temperature and an initial stress equal to, or slightly lower than the stress in creeping. The course of relaxation at different accumulated plastic deformation until destruction of the specimen was clarified by alternating creeping and relaxation tests. The Ref. 4 by V.I. Danilovskaya, G.M. Ivanova, and Yu.N. Rabotnov, Izvestiya AN SSSR, OTN, No. 5 (1955) is mentioned in this connection. Fig. 1, shows the relaxation curves (1-6) and curve 7 characterizing the plastic deformation in all creeping and relaxation cycles of the same specimen of EI612 steel; Fig. 1,4 shows the same curves for another specimen of the same steel. Every creeping cycle of the first specimen was continued until reaching the plastic deformation of 0.1 - 0.3%, of the second specimen up to 0.7%; in the former case, the Creeping cycle lasted 50-80 hr. in the latter case, 40 hr, the relaxation

25357 \$/032/61/027/006/008/018 B124/B203

Tests for relaxation ...

cycles lasted 200-450, and 300-600 hr, respectively. Fig.2 illustrates the relation between residual stress and plastic deformation in creeping before each relaxation cycle. The formation of plastic deformation in relaxation, or relaxation and creeping, effects a damage to the steel which, in turn, accelerates the course of relaxation. The degree of damage can be determined by the quantity $\epsilon_{pd}/\epsilon_{d}$, where ϵ_{pd} is the arbitrarily (by relaxation, creeping, or relaxation and creeping) accumulated plastic deformation before starting the relaxation test, and s is the elongation at break in creeping, determining the plasticity reserve of the steel. The quantity 1 - E pd/& characterizes the plasticity reserve conserved. The relation between relaxation stability ($\sigma_{\rm rst}/\delta_{\rm d}$) and damage ($\iota_{\rm pd}/\delta_{\rm d}$) or plasticity reserve (1 - $\iota_{\rm pd}/\delta_{\rm d}$) of EI612 steel is given in Fig.3. The elongation at break in the last relaxation of creeping cycle was 1.1 - 2.4%. In 28KhVFTs steel, the stress drop is delayed and the relaxation stability rises with increasing accumulated plastic deformation. In 20Kh1M1F1 steel, the relaxation stability rises continuously with plastic deformation almost to the instant of destruction. In austenitic steel EI612, the relaxation Card 3/9

25357

S/032/61/027/006/008/018 B124/B203

stability drops continuously with rising plastic deformation and consumption of the plasticity reserve, whereas in perlite steels with high (28KhVFTs) and low (20Kh1M1F1) plasticity reserves it rises, and reaches a maximum near the destruction limit. In austenitic steel, the damage increases with plastic deformation, and the intergranular cracks enlarge under the action of stress, which accelerates relaxation, while the damages in perlite steels may "heal on their own", particularly at steadily dropping stress. There are 5 figures, 1 table, and 4 Soviet-bloc references.

ASSOCIATION: Tsentral nyy kotloturbinnyy institut im. I. I. Polzunova (Central Boiler and Turbine Institute imeni I. I. Polzunov)

Card 4/9

Tests for relaxation ...

55000

S/129/62/000/004/002/010 E193/E383

18.1150

L. Ya. Candidate of Technical Sciences AUTHOR:

Relaxation stability of steels 3 1612 (EI612) and TITLE:

20X1MID1 (20KhlM1F1) in tension and fracture

Metallovedeniye i termicheskaya obrabotka metallov, PERIODICAL: no. 4, 1962, 6 - 13

The object of the present investigation was to assess the notch sensitivity of steels EI612 and 20KhlM1F1 by determining the, so-called, "plasticity reserve" of these materials. To this end stress relaxation was studied on smooth specimens (12 mm diameter, 155 mm gauge length), tested to fracture in tension. The composition and mechanical properties of the steels studied are given in Table 1. Three types of tests were carried 1) specimens, heated to a given test temperature, were loaded and held under conditions of constant strain for 700 -1 000 h, after which the stress was increased to the initial level; 2) specimens were tested to fracture under conditions of cyclic relaxation which entailed increasing the stress to the initial level every 100 - 120 h; 3) specimens were tested under Card 1/4

S/129/62/000/004/002/010 E193/E383

Relaxation stability

conditions of alternating relaxation and creep. The results, which are reproduced graphically, can be summarized as follows. Accumulation of plastic strain accelerates the relaxation process in the austemitic steel EI612; in the case of pearlitic steel 20KhlMlFl the resistance to relaxation continuously increases, the decrease in stress being delayed until practically the entire "plasticity reserve" (0.90 - 0.95%) is used up. b) Fracture of specimens tested under conditions of stress relaxation (alone or alternating with periods of creep) takes place as a result of the entire "plasticity reserve" being used up. In the case of unnotched specimens, tested under conditions of stress relaxation, the extent to which the specimen has progressed towards fracture can be characterized by the ratio, where $\epsilon_{n,n}$ denotes the plastic strain at a elongation at the moment of fracture. given moment and This ratio can serve as a criterion of vulnerability of the specimen whose "plasticity reserve" is given by $1 - \epsilon_{nJ}/\delta_{p}$.

Card 2/4